Motor Sizing Example BJ Furman 19OCT2010

Reference: Maxon 02/03 Catalog

 $J_L := 120000 \cdot \text{gm} \cdot \text{cm}^2$   $J_L = 0.012 \text{ kg} \cdot \text{m}^2$  RPM  $:= \frac{2 \cdot \pi}{60 \cdot \text{s}}$  unit definition for RPM  $T_{fric} := 300 \cdot 10^{-3} \cdot N \cdot m$   $T_{ext} := 0 \cdot N \cdot m$   $V_S := 24 \cdot V$  Supply voltage  $i_{supply\_max} := 5 \cdot A$  $\omega_{\text{load}} := 60 \cdot \text{RPM}$   $\omega_{\text{load}} = 6.283 \frac{\text{rad}}{2}$  Maximum rotational speed of the load Motion Profile  $t_{accel} \coloneqq 0.5 \cdot s \quad t_{slew} \coloneqq 2.5 \cdot s - t_{accel} \qquad t_{dec} \coloneqq 3.0 \cdot s - 2.5 \cdot s \quad t_{dwell} \coloneqq 3.7 \cdot s - 3.0 \cdot s \quad t_{cycle} \coloneqq 3.7 \cdot s = 3.7 \cdot$  $\alpha := \frac{\omega_{load}}{t_{accel}} \qquad \left| \alpha = 12.566 \frac{rad}{s^2} \right| \qquad \text{Angular acceleration of the load}$ Find Tpeak, which must be delivered to the load  $T_{peak\_load} := J_{L} \cdot \alpha + T_{fric} + T_{ext} \qquad T_{peak\_load} = 0.451 \,\text{N} \cdot \text{m}$ The motor chosen needs to be capable of delivering at least this torque to the load. Find the RMS torque, which must be delivered to the load  $T_{accel} := J_L \cdot \alpha$   $T_{accel} = 0.151 \, \text{N} \cdot \text{m}$   $T_{slew} := T_{fric} T_{slew} = 0.3 \, \text{N} \cdot \text{m}$  $T_{dec} := -T_{peak\_load} + T_{fric}$   $T_{dec} = -0.151 \,\text{N} \cdot \text{m}$   $T_{dwell} := 0$  $T_{RMS} := \sqrt{\frac{1}{t_{cycle}} \cdot \left(t_{accel} \cdot T_{peak\_load}^2 + t_{slew} \cdot T_{slew}^2 + t_{dec} \cdot T_{dec}^2 + t_{dwell} \cdot T_{dwell}^2\right)}$  $T_{RMS} = 0.281 \,\mathrm{N \cdot m}$  T<sub>rms</sub> is the effective continuous torque  $P_{max} := T_{peak\_load} \cdot \omega_{load}$   $P_{max} = 2.832 \text{ W}$ The motor chosen needs to be capable of delivering at least about 3 W. This number can be used to 'get in the ballpark' for choosing a motor. Select the gearing  $\omega_{\max\_gear} := 6000 \cdot \text{RPM}$   $G_{red\_max} := \frac{\omega_{max\_gear}}{\omega_{load}}$   $G_{red\_max} = 100$  The gear reduction cannot be larger than  $G_{red\_max}$ , or else the motor won't be able to rotate the load up to 60 RPM The gearhead must be able to handle  $T_{peak\_load}$  and  $T_{RMS}$ 

 $G_{red} \coloneqq 84$   $\eta_G \coloneqq 0.59$  Of the available gearheads listed in the catalog, a 22mm dia planetary gear type will handle the peak and RMS torques. The closest ratio available that is less than  $G_{red_max}$  is 84:1. It has an efficiency of 59%.

### Find speed and torque *at the motor shaft* (i.e., "reflected" through the gearhead)

$$\omega_{mot} := G_{red} \cdot \omega_{load} \qquad \omega_{mot} = 5.04 \times 10^{3} \text{RPM}$$

$$T_{RMS\_mot} := \frac{T_{RMS}}{G_{red} \cdot \eta_G} \qquad T_{RMS\_mot} = 5.678 \times 10^{-3} \text{N} \cdot \text{m}$$

$$T_{mot\_max} := \frac{T_{peak\_load}}{G_{red} \cdot \eta_G} \qquad T_{mot\_max} = 9.096 \times 10^{-3} \text{N} \cdot \text{m}$$

Use these torque values to find a motor from the catalog. Note that these are <u>minimum</u> values. Your choice of a motor should allow for some margin (at least 20% beyond the minimum values). A Maxon A-max 22mm dia, 6W type will work (actually several model numbers in this category will work.) Select the most appropriate one by looking at the operating point on the speed-torque curve and the margin for speed control.

## Select the motor winding

$$ST_{grad} := 480 \cdot \frac{RPM}{N \cdot m \cdot 10^{-3}}$$

For the A-max 22mm dia, 6W type motors in the catalog, this is the average speed-torque gradient (i.e., the slope of the operating line in the torque-speed graph.)

$$\begin{split} & \omega_{NL\_targ} \coloneqq \omega_{mot} + ST_{grad} \cdot T_{mot\_max} & \omega_{NL\_targ} = 9.406 \times 10^{3} \text{RPM} & \text{This is the no-load speed corresponding to the speed-torque line that passes through the operating point of the motor: (T_{peak\_mot}, \omega_{mot}) \\ & V_{wind} \coloneqq V_{S} - 6 \cdot V & V_{wind} = 18 \text{ V} & \text{This is the maximum voltage available to be applied to the motor. The speed-torque line that passes available to be applied to the motor. The speed-torque line that passes available to be applied to the motor. The speed-torque line that passes available to be applied to the motor. The speed-torque line that passes available to be applied to the motor. The speed-torque line that passes available to be applied to the motor. The speed-torque line that passes available to be applied to the motor. The speed-torque line that passes available to be applied to the motor. The speed-torque line that passes available to be applied to the motor. The speed-torque line that passes available to be applied to the motor. The speed-torque line that passes available to be applied to the motor. The speed-torque line that passes available to be applied to the motor. The speed-torque line that passes available to be applied to the motor. The speed-torque line torque line to the motor passes available to be applied to the motor. The speed-torque line torque line$$

 $V_{wind} = 18 V$  This is the maximum voltage available to be applied to the motor. The drive electronics (power amplifier) will have a voltage drop of about 6V, according to Maxon.

k <sub>speed</sub> := -	$\frac{\omega_{\text{NL}_{targ}}}{V_{\text{wind}}}$	$k_{\text{speed}} = 522.559 \frac{\text{RPM}}{\text{V}}$	

This is the <u>minimum</u> speed constant that the motor must have. (The speed constant is the reciprocal of the back EMF constant,  $K_E$ .)

Looking at the catalog page for the A-max, 22mm, 6W motors, model 110163 would just about meet the requirements, but with almost no margin. Choose motor **110162** instead, because it has a slightly larger speed constant, so it will have more than the desired 20% margin for meeting the speed requirements given that only 18V is available for driving the motor.

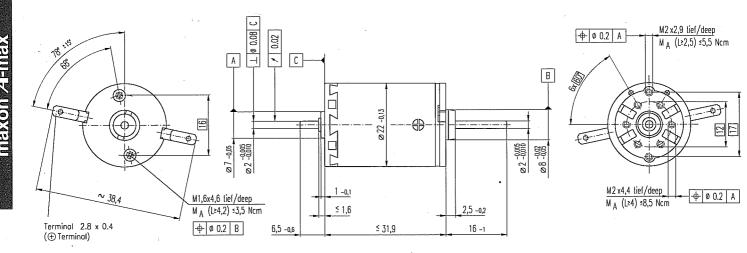
$$K_T := 13.9 \cdot 10^{-3} \cdot N \cdot \frac{m}{A}$$
 Torque constant for the 110162 motor

Check the maximum current

$$I_{max} \coloneqq \frac{T_{mot\_max}}{K_T} \qquad I_{max} = 0.654 \text{ A} \quad \text{Imax is lower than 2A of that the power amplifier can deliver.}$$

It would also be a good idea to check the temperature rise under the ambient operating conditions. More information on how to do this can be found in the Maxon catalog.

# **1-max 22** Ø22 mm, Graphile Drushes, o wall



#### Stock program

Standard program

**Order Number** 

Ø22 mm 0.1 - 0.6 Nm

Ø22 mm 0.5 - 1.0 Nm

Ø22 mm 0.5 - 2.0 Nm

Ø24 mm 0.1 Nm

			110156	110158	110159	110160	110161	110162	110163	110164	110165	110166	110167	110168	
10	tor Data					신속 한 문	14.12.51								
1	Assigned power rating	W	6.0	6.0	6.0	6.0	6.0	6.0	6.0	6.0	6.0	6.0	6.0	6.0	
2	Nominal voltage	Volt	6.0	9.0	9.0	12.0	12.0	15.0	18.0	24.0	24.0	36.0	48.0	48.0	
3	No load speed	rpm	9240	9700	8520	10200	9190	10100	9780	10500	8490	9640	9120	8210	
4	Stall torque	mNm	15.6	19.7	18.0	22.0	19.7	21.9	21.4	23.4	18.8	21.1	19.3	17.7	
5	Speed / torque gradient	rpm / mNm	624	511	490	477	482	472	468	462	464	468	484	476	
6	No load current	mA	83	58	50	46	41	36	29	24	18	14	10	9	
7	Starting current	mA	2640	2300	1850	2020	1630	1580	1250	1100	716	606	395	327	
8	Terminal resistance	Ohm	2.27	3.91	4.86	5.95	7.38	9.49	14.4	21.8	33.5	59.4	122	147	
9	Max. permissible speed	rpm	9800	9800	9800	9800	9800	9800	9800	9800	9800	9800	9800	9800	
10	Max. continuous current	mA	1080	841	756	680	612	539	439	356	287	216	151	137	
11	Max. continuous torque	mNm	6.37	7.19	7.36	7.43	7.40	7.47	7.51	7.56	7.55	7.51	7.38	7.45	
12	Max. power output at nominal voltage	mW	3480	4740	3820	5640	4550	5580	5340	6300	4070	5210	4520	3730	
13	Max. efficiency	%	65	69	69	71	70	72	72	73	71	72	71	70	
14	Torque constant	mNm / A	5.90	8.55	9.73	10.9	12.1	13.9	17.1	21.2	26.3	34.8	49.0	54.3	
15	Speed constant	rpm / V	1620	1120	981	875	790	689	558	450	364	274	195	176	
16	Mechanical time constant	ms	25	22	21	20	20	20	19	19	19	18	18	18	
17	Rotor inertia	gcm <sup>2</sup>	3.81	4.03	4.09	4.06	3.97	3.96	3.90	3.89	3.84	3.77	3.63	3.68	
18	Terminal inductance	mH	0.11	0.22	0.29	0.36	0.45	0.59	0.89	1.37	2.10	3.69	7.30	8.98	
19	Thermal resistance housing-ambient	K/W	20	20	20	20	20	20	20	20	20	20	20	20	
20	Thermal resistance rotor-housing	K/W	6.0	6.0	6.0	6.0	6.0	6.0	6.0	6.0	6.0	6.0	6.0	6.0	

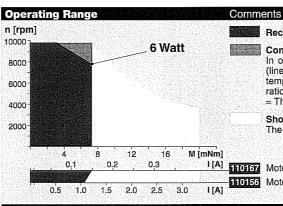
#### Specifications

Axial play	0.05 - 0.15 mm
<ul> <li>Max. sleeve bearing loads axial (dynamic) radial (5 mm from flange) Press-fit force (static) (static, shaft supported)</li> </ul>	1.0 N 2.8 N 80 N 440 N
<ul> <li>Max. ball bearing loads axial (dynamic) radial (5 mm from flange) Press-fit force (static) (static, shaft supported)</li> </ul>	3.3 N 12.3 N 45 N 440 N
<ul> <li>Radial play sleeve bearing</li> </ul>	0.012 mm
<ul> <li>Radial play ball bearing</li> </ul>	0.025 mm
<ul> <li>Ambient temperature range</li> </ul>	-30 / +85°C
<ul> <li>Max. rotor temperature</li> </ul>	+125°C
Number of commutator segments	s 9
<ul> <li>Weight of motor</li> </ul>	54 g

Weight of motor Values listed in the table are nominal. . For applicable tolerances (see page 43). For additional details please use the maxon selection program on the enclosed CD-Rom.

Options: Ball bearings in place of sleeve bearings and pigtails in place of terminals.





HOIG7 Motor with high resistance winding HOLES Motor with low resistance winding

Recommended operating range

**Continuous operation** 

ration at 25°C ambient. = Thermal limit.

Short term operation

Details on page 49

In observation of above listed thermal resistances

(lines 19 and 20) the maximum permissible rotor temperature will be reached during continuous ope-

The motor may be briefly overloaded (recurring).

