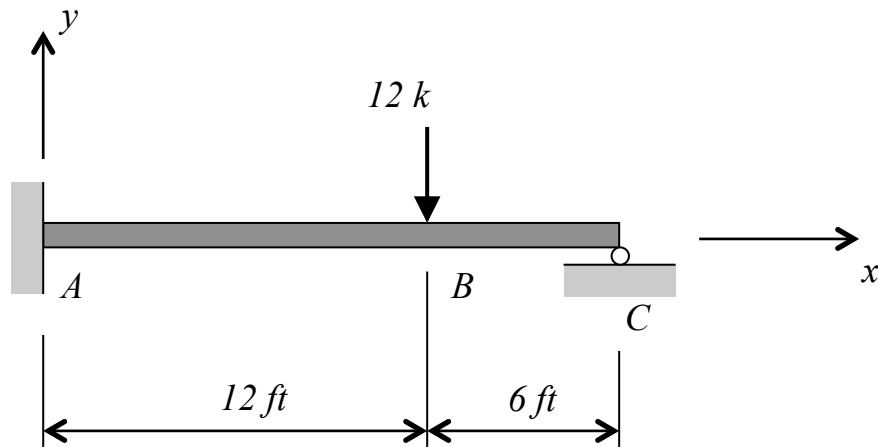


CE 160 Indeterminate Beam Lab Problem



The beam analyzed by the direct stiffness method in Lab #11 is statically indeterminate to the first degree. Recall that the beam has the following properties:

Section	I	E
W8x10	30.8 in ⁴	29000 ksi

Using the force method of analysis, define the released structure to be a simply supported beam with a pin at A and roller and C. This released structure also defines the redundant to be the moment reaction at the fixed support at A.

1. Set up the released problem and find the slope at A for the released problem. The tabulated solutions attached to the last page of this note package will be useful to you. Write your answer below:

$$\theta_{A0} =$$

2. Set up the redundant problem and find the flexibility coefficient at point A by applying the redundant at a unit value at A. Use the attached tabulated solutions and write your answer below:

$$\alpha_{AA} =$$

3. Enforce compatibility at point A and solve for the bending moment reaction at A in the indeterminate problem. Write your solution below:

$$\theta_{A0} + M_A \alpha_{AA} = 0$$

$$M_A =$$

4. Use equilibrium to find the two force reactions at A and C and write your results below:

$$A_y =$$

$$C_y =$$

5. From your results in Steps 3 and 4, draw the loading, shear, and bending moment diagrams for the indeterminate beam below:

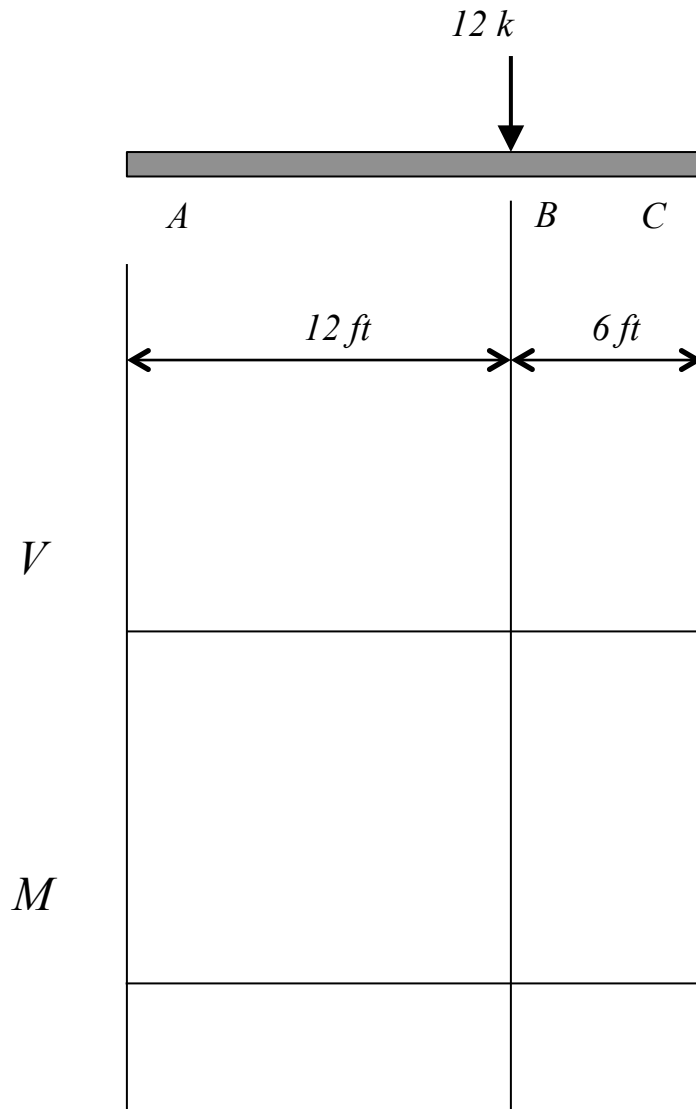
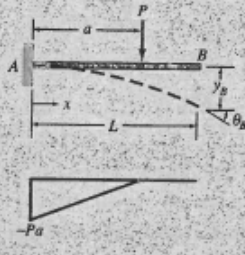
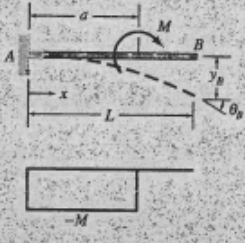
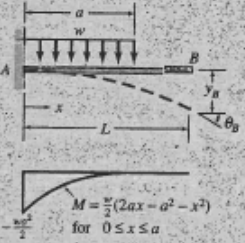
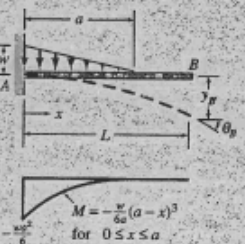
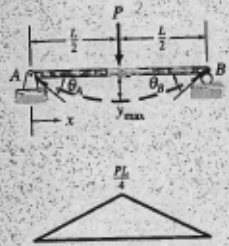
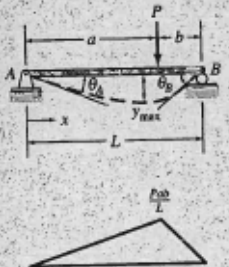
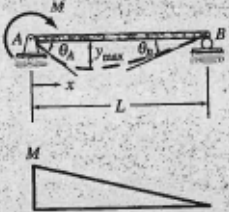


Table to aid in finding θ_{A0} and α_{AA} in Steps 1 and 2.

Beam, Loading, and Bending Moment Diagram	Equations for Slope and Deflection
	$0 \leq x \leq a:$ $\theta = \frac{P}{2EI}(x^2 - 2ax)$ $y = \frac{P}{6EI}(x^3 - 3ax^2)$ $a \leq x \leq L:$ $\theta = -\frac{Pa^2}{2EI}$ $y = \frac{Pa^2}{6EI}(a - 3x)$ $\theta_B = -\frac{Pa^2}{2EI}; \quad y_B = -\frac{Pa^2}{6EI}(3L - a)$
	$0 \leq x \leq a:$ $\theta = -\frac{Mx}{EI}$ $y = -\frac{Mx^2}{2EI}$ $a \leq x \leq L:$ $\theta = -\frac{Ma}{EI}$ $y = \frac{Ma}{2EI}(a - 2x)$ $\theta_B = -\frac{Ma}{EI}; \quad y_B = -\frac{Ma}{2EI}(2L - a)$
	$0 \leq x \leq a:$ $\theta = \frac{w}{6EI}(3ax^2 - 3a^2x - x^3)$ $y = \frac{w}{24EI}(4ax^3 - 6a^2x^2 - x^4)$ $a \leq x \leq L:$ $\theta = -\frac{wa^2}{6EI}$ $y = \frac{wa^3}{24EI}(a - 4x)$ $\theta_B = -\frac{wa^2}{6EI}; \quad y_B = -\frac{wa^3}{24EI}(4L - a)$
	$0 \leq x \leq a:$ $\theta = \frac{w}{24EIa}(x^4 - 4ax^3 + 6a^2x^2 - 4a^3x)$ $y = \frac{w}{120EIa}(x^5 - 5ax^4 + 10a^2x^3 - 10a^3x^2)$ $a \leq x \leq L:$ $\theta = -\frac{wa^3}{24EI}$ $y = \frac{wa^3}{120EI}(-5x + a)$ $\theta_B = -\frac{wa^3}{24EI}; \quad y_B = -\frac{wa^3}{120EI}(5L - a)$

Beam, Loading, and Bending Moment Diagram	Equations for Slope and Deflection
	$0 \leq x \leq \frac{L}{2} :$ $\theta = \frac{P}{16EI} (4x^2 - L^2)$ $y = \frac{P}{48EI} (4x^3 - 3L^2x)$ $\theta_A = -\frac{PL^2}{16EI}; \quad \theta_B = \frac{PL^2}{16EI}$ $y_{\max} = -\frac{PL^3}{48EI}$
	$0 \leq x \leq a :$ $\theta = \frac{Pb}{6EI} (3x^2 + b^2 - L^2)$ $y = \frac{Pb}{6EI} (x^3 + b^2x - L^2x)$ $a \leq x \leq L :$ $\theta = \frac{Pa}{6EI} [L^2 - a^2 - 3(L-x)^2]$ $y = \frac{Pa(L-x)}{6EI} (x^2 + a^2 - 2Lx)$ $\theta_A = -\frac{Pb}{6EI} (L^2 - b^2)$ $\theta_B = \frac{Pa}{6EI} (L^2 - a^2)$ <p>For $a \geq b :$</p> $y_{\max} = -\frac{Pb}{9\sqrt{3}EI} (L^2 - b^2)^{3/2}$ $\text{at } x = \left(\frac{L^2 - b^2}{3} \right)^{1/2}$
	$\theta = -\frac{M}{6EI} (3x^2 - 6Lx + 2L^2)$ $y = -\frac{M}{6EI} (x^3 - 3Lx^2 + 2L^2x)$ $\theta_A = -\frac{ML}{3EI}; \quad \theta_B = \frac{ML}{6EI}$ $y_{\max} = -\frac{ML^2}{9\sqrt{3}EI}$ $\text{at } x = L \left(1 - \frac{1}{\sqrt{3}} \right)$